New PDEs governing both fluids and solids Symmetric-hyperbolic balance laws to model viscoelastic flows of Maxwell fluids

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Viscoelastic flows, Maxwell fluids & hyperbolic PDEs



To compute unequivocal solutions to Cauchy problems we propose a *symmetric-hyperbolic system of balance laws* that contains $\lambda \stackrel{\diamond}{\tau} + \tau = 2\mu D(u)$, and that models denoting $D(u) = \frac{1}{2} (\nabla u + \nabla u^T) \equiv \frac{1}{2} (L + L^T), \stackrel{\diamond}{\tau} \equiv \stackrel{\nabla}{\tau} = \partial_t \tau + (u \cdot \nabla) \tau - (\nabla u) \tau - \tau (\nabla u)^T$

• Hookean solids when $\lambda, \mu \equiv G\lambda \to \infty$: where $\tau = G(FF^T - I), (\partial_t + u \cdot \nabla)F = LF \Rightarrow \stackrel{\diamond}{\tau} \equiv \stackrel{\nabla}{\tau} \equiv \partial_t \tau + (u \cdot \nabla)\tau - L\tau - \tau L^T$

• Newtonian fluids when $\lambda, \lambda/\mu \equiv 1/G \rightarrow 0$: $\tau = 2\mu D(u)$

Outline

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1 Setting the constitutive modelling issue

Prom anisotropic elastodynamics to viscoelastic fluids



Continuum Mechanics

We look for $\mathbb{R}^d = \{ \boldsymbol{x} = \phi_t^i(\boldsymbol{a})\boldsymbol{e}_i, \ \boldsymbol{a} = \boldsymbol{a}^{\alpha}\boldsymbol{e}_{\alpha} \} \quad \forall t \in [0, T), \text{ i.e.}$

velocity $\mathbf{u} \equiv \partial_t \phi_t$ and deformation gradient $\mathbf{F} \equiv \partial_\alpha \phi_t^i \mathbf{e}_i \otimes \mathbf{e}^\alpha$

$$\partial_t F^i_\alpha - \partial_\alpha u^i = 0 \tag{1}$$

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$$\partial_t |\boldsymbol{F}| - \partial_\alpha \left(\hat{F}^i_\alpha \, \boldsymbol{u}^i \right) = \mathbf{0}$$
 (2)

$$\partial_t \hat{F}^i_{\alpha} + \sigma_{ijk} \sigma_{\alpha\beta\gamma} \partial_\beta \left(F^j_{\gamma} u^k \right) = 0$$
(3)

where |F| and \hat{F} denote *determinant* and *cofactor matrix* of F

while Piola's identities hold ($\sigma_{\alpha\beta\gamma}$ is Levi-Civita's symbol)

$$\sigma_{\alpha\beta\gamma}\partial_{\beta}F_{\gamma}^{i} = \mathbf{0} = \partial_{\alpha}\hat{F}_{\alpha}^{i} \quad \forall i$$
(4)

 $(\partial_b F_a^i = \partial_a F_b^i)$

Newtonian physics

We require balance of energy

using material coordinates i.e.

$$\hat{\rho}\partial_t \left(\frac{|\boldsymbol{u}|^2}{2} + \boldsymbol{e}\right) = \partial_\alpha \left(\boldsymbol{S}_i^\alpha \boldsymbol{u}^i\right) + \hat{\rho}f_i \boldsymbol{u}^i \tag{5}$$

where stored energy $e(\mathbf{F})$ defines first Piola-Kirchoff stress **S**

$$S_i^{\alpha} = \hat{\rho} \partial_{F_{\alpha}^i} \boldsymbol{e} \,. \tag{6}$$

We require momentum balance in fact, i.e. in Cartesian system

$$\hat{\rho}\partial_t u_i = \partial_\alpha S_i^\alpha + \hat{\rho} f_i \tag{7}$$

by Galilean invariance. Here, we also assume $\hat{\rho}$ constant.

Lagrangian description

Then, computable motions $\phi_t(\mathbf{a})$ are defined on specifying i) *constitutive relations* $e(\mathbf{F})$, strictly convex in \mathbf{F} e.g. like

$$e(\boldsymbol{F}) = \frac{c_1^2}{2} (F_\alpha^k F_\alpha^k - d)$$
(8)

 $(c_1^2 \equiv G > 0 \text{ is Lamé's second coefficient or shear modulus})$ hence $\boldsymbol{S}(\boldsymbol{F}) = c_1^2 \boldsymbol{F}^T$ in the (symmetric-hyperbolic) system

$$\partial_t \boldsymbol{F}^T = \boldsymbol{\nabla}_{\boldsymbol{a}} \boldsymbol{u}$$
 (9)

$$\hat{\rho}\partial_t \boldsymbol{u} = \operatorname{div}_{\boldsymbol{a}} \boldsymbol{S} + \hat{\rho} \boldsymbol{f}$$
 (10)

plus ii) *initial conditions* for (9–10), e.g. in $[H^{s}(\mathbb{R}^{d})]^{3d}$ (whatever $s \in \mathbb{R}, \forall T > 0$ here: (9–10) is linear !)

Neo-Hookean materials

A more realistic constitutive relation (for rubber, resine...) is

$$\boldsymbol{e}(\boldsymbol{F}) = \frac{c_1^2}{2}(\boldsymbol{F}:\boldsymbol{F}-\boldsymbol{d}) - \frac{d_1^2}{1-\gamma}|\boldsymbol{F}|^{1-\gamma}$$
(11)

(where d_1^2 is Lamé's first coefficient). Properties of (11):

e(*F*) is *polyconvex* in *F* as soon as *γ* > 1

 $\textbf{\textit{e}}(\textbf{\textit{F}})\equiv\tilde{\textbf{\textit{e}}}(|\textbf{\textit{F}}|,\textbf{\textit{F}}) \text{ convex in } |\textbf{\textit{F}}|,\textbf{\textit{F}}$

well defining solutions with $S_i^{\alpha}(\mathbf{F}) = \hat{\rho} c_1^2 F_{\alpha}^i - \hat{\rho} d_1^2 |\mathbf{F}|^{-\gamma} \hat{F}_{\alpha}^i$ to

$$\partial_t \boldsymbol{F}^T = \boldsymbol{\nabla}_{\boldsymbol{a}} \boldsymbol{u}$$
 (12)

$$\partial_t |\boldsymbol{F}| = \operatorname{div}_{\boldsymbol{a}}(\boldsymbol{u} \cdot \hat{\boldsymbol{F}})$$
 (13)

$$\partial_t \boldsymbol{u} = \operatorname{div}_{\boldsymbol{a}}(\boldsymbol{S}/\hat{\rho}) + \boldsymbol{f}$$
 (14)

Sac

• e(F) is material-frame indifferent

$$oldsymbol{e}(oldsymbol{F})\equivar{oldsymbol{e}}(oldsymbol{C},|oldsymbol{C}|)$$
 where $oldsymbol{C}=C_{lphaeta}oldsymbol{e}^{lpha}\otimesoldsymbol{e}^{eta},C_{lphaeta}=F^i_{lpha}F^i_{eta},$

ē is monotone convex in each argument for polyconvexity

Eulerian description

Smooth solutions to (11–14) preserving $\nabla_{a} \times F^{T} = 0$ are equivalently (smooth) solutions preserving div(ρF^{T}) = 0 to

$$\partial_t \left(\rho \boldsymbol{u} \right) + \operatorname{div} \left(\rho \boldsymbol{u} \otimes \boldsymbol{u} - \boldsymbol{\sigma} \right) = \rho \boldsymbol{f}$$
 (15)

$$\partial_t (\rho \boldsymbol{F}) - \boldsymbol{\nabla} \times \left(\rho \boldsymbol{F}^T \times \boldsymbol{u} \right) = \boldsymbol{0}$$
 (16)

$$\partial_t \rho + \operatorname{div}\left(\rho \boldsymbol{u}\right) = \boldsymbol{0}$$
 (17)

using mass density $ho=\hat{
ho}/|{m F}|$ and Cauchy stress

$$\sigma^{ij} := |\boldsymbol{F}|^{-1} \boldsymbol{S}^{i\alpha} \boldsymbol{F}_{\alpha}^{j} \equiv \rho \boldsymbol{c}_{1}^{2} \boldsymbol{F}_{\alpha}^{i} \boldsymbol{F}_{\alpha}^{j} - \rho \boldsymbol{d}_{1}^{2} \left(\frac{\rho}{\hat{\rho}}\right)^{\gamma} \delta^{ij}.$$

It allows one to define *isentropic*, time-reversible motions of "solids", isotropic (motions depend only on c_1^2 , d_1^2 , not direction)

Fluid motions

Within liquids, stress are mostly spheric i.e. $\sigma = -pI$ like in the famous barotropic case $e(\mathbf{F}) = \frac{C_0}{\gamma - 1} \rho^{\gamma - 1}$, $p = C_0 \rho^{\gamma}$

$$\partial_t \left(\rho \boldsymbol{u} \right) + \operatorname{div} \left(\rho \boldsymbol{u} \otimes \boldsymbol{u} - \boldsymbol{\sigma} \right) = \rho \boldsymbol{f}$$
 (18)

$$\partial_t \rho + \operatorname{div}\left(\rho \boldsymbol{u}\right) = \boldsymbol{0}$$
 (19)

well posed – though not in Lagrangian description. Anyway, real liquids are also viscous, and flow non-reversibly.

Newtonian fluids $\sigma = -p\mathbf{I} + \tau$, $\tau = 2\mu \mathbf{D}(\mathbf{u})$ produce entropy, but lack shear elasticity as in e.g. gels, letting alone that shear then propagates at infinite speed and fails at

Fluids (micro-)structure

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Rheology of solids & liquids depends on (micro-)structure

Use Maxwell constitutive relation with structural variable au ?

Objective suspension flow models $\lambda \stackrel{\diamond}{\tau} + \tau = 2\mu \mathbf{D}(\mathbf{u})$ where e.g. $\stackrel{\diamond}{\tau} \equiv \stackrel{\nabla}{\tau} := \partial_t \tau + (\mathbf{u} \cdot \nabla) \tau - (\nabla \mathbf{u}) \tau - \tau (\nabla \mathbf{u})^T$ are not well-posed.

The *linearized* system is hyperbolic if $\mathbf{c} := \mathbf{I} + \frac{\lambda}{\mu} \tau > 0$, but the *nonlinear* system has no conservative formulation.

Let's use a *structural tensor* $\mathbf{A} = \mathbf{A}^T > 0$ (like in plastic solids !) modelling anisotropy in stored energy through tr(\mathbf{AC}).

Outline

Setting the constitutive modelling issue

2 From anisotropic elastodynamics to viscoelastic fluids



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Anisotropic elastodynamics

Defects inducing anisotropy in solids can be modelled on modifying elastodynamics system preserving $div(\rho F) = 0$

$$\partial_t (\rho \boldsymbol{u}) + \operatorname{div} (\rho \boldsymbol{u} \otimes \boldsymbol{u} - \boldsymbol{\sigma}) = \rho \boldsymbol{f}$$

$$\partial_t (\rho \boldsymbol{F}) - \boldsymbol{\nabla} \times \left(\rho \boldsymbol{F}^T \times \boldsymbol{u} \right) = \boldsymbol{0}$$

$$\partial_t \rho + \operatorname{div} (\rho \boldsymbol{u}) = \boldsymbol{0}$$
 (20)

where $\boldsymbol{\sigma} := \rho \left(\partial_{\boldsymbol{F}} \boldsymbol{e}\right) \cdot \boldsymbol{F}^{T}$ is given by $\boldsymbol{e}(\boldsymbol{F}) = \bar{\boldsymbol{e}}(\boldsymbol{C}, |\boldsymbol{C}|)$ material-frame indifferent, polyconvex in \boldsymbol{F} . Introducing a structure parameter $\boldsymbol{A} = \boldsymbol{F}_{\rho}^{-1} \cdot \boldsymbol{F}_{\rho}^{-T} > 0$ in e.g.

$$\boldsymbol{e}(\boldsymbol{F}) = \frac{c_1^2}{2} (\operatorname{tr}(\boldsymbol{F} \cdot \boldsymbol{A} \cdot \boldsymbol{F}^{\mathsf{T}}) - \boldsymbol{d}) - \frac{d_1^2}{1 - \gamma} |\boldsymbol{F}|^{1 - \gamma}$$
(21)

(still polyconvex in \mathbf{F} !) yields $\boldsymbol{\sigma} = \rho c_1^2 \mathbf{F} \cdot \mathbf{A} \cdot \mathbf{F}^T - p\mathbf{I}$ with *strain* $\mathbf{F} \cdot \mathbf{A} \cdot \mathbf{F}^T$ like in [Green, Naghdi 1965] [Lee, Liu 1967]

Maxwell fluids with hyperbolic PDEs

Assuming (20) and a modified neo-Hookean stored energy with structure parameter A(t, x) as in (21),

Maxwell fluids $\lambda \stackrel{\diamond}{\tau} + \tau = 2\mu D(u)$ result from requiring $\mu = \lambda c_1^2$

$$\tau = \rho c_1^2 (\boldsymbol{F} \cdot \boldsymbol{A} \cdot \boldsymbol{F}^T - \boldsymbol{I})$$

$$\lambda (\partial_t + \boldsymbol{u} \cdot \boldsymbol{\nabla}) \boldsymbol{A} + \boldsymbol{A} = \boldsymbol{F}^{-1} \boldsymbol{F}^{-T}$$
(22)

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$$\stackrel{\diamond}{\tau} = \partial_t \boldsymbol{\tau} + (\boldsymbol{u} \cdot \boldsymbol{\nabla}) \boldsymbol{\tau} - \boldsymbol{\nabla} \boldsymbol{u} \cdot \boldsymbol{\tau} - \boldsymbol{\tau} \cdot \boldsymbol{\nabla} \boldsymbol{u}^T + (\operatorname{div} \boldsymbol{u}) \boldsymbol{\tau} \,. \tag{23}$$

Theorem (Lieb, 1973) $(\boldsymbol{F}, \boldsymbol{Y}) \in \mathbb{R}^{d \times d} \times SDP^{d \times d} \rightarrow tr\left(\boldsymbol{F} \boldsymbol{Y}^{-\frac{1}{2}} \boldsymbol{F}^{T}\right)$ is convex

By Godunov-Mock theorem, the system of conservation laws (20–22) is symmetric hyperbolic when $div(\rho F) = 0$ [Boyaval M2AN 2021]

Thermodynamics consistency

The solutions preserving $div(\rho F) = 0$ to

$$\partial_{t} (\rho \boldsymbol{u}) + \operatorname{div} (\rho \boldsymbol{u} \otimes \boldsymbol{u} - \boldsymbol{\sigma}) = \rho \boldsymbol{f}$$

$$\partial_{t} (\rho \boldsymbol{F}) - \boldsymbol{\nabla} \times (\rho \boldsymbol{F}^{T} \times \boldsymbol{u}) = \boldsymbol{0}$$

$$\partial_{t} \rho + \operatorname{div} (\rho \boldsymbol{u}) = \boldsymbol{0}$$

$$\partial_{t} \boldsymbol{A} + \boldsymbol{u} \cdot \boldsymbol{\nabla} \boldsymbol{A} = \frac{1}{\lambda} (\boldsymbol{F}^{-1} \boldsymbol{F}^{-T} - \boldsymbol{A})$$
(24)

 $\sigma = \rho c_1^2 \mathbf{F} \cdot \mathbf{A} \cdot \mathbf{F}^T - \rho \mathbf{I} = \tau - \tilde{\rho} \mathbf{I}$ satisfy the energy balance

$$\partial_t \boldsymbol{E} + \operatorname{div}\left(\boldsymbol{E}\boldsymbol{u} - \boldsymbol{\sigma} \cdot \boldsymbol{u}\right) = \rho \boldsymbol{f} \cdot \boldsymbol{u} + \frac{\rho c_1^2}{2\lambda} (\boldsymbol{I} - \boldsymbol{c}^{-1}) : (\boldsymbol{c} - \boldsymbol{I}) \quad (25)$$

using $\boldsymbol{c} = \boldsymbol{F} \boldsymbol{A} \boldsymbol{F}^T \in \boldsymbol{S}^{+,*}, \ \boldsymbol{E} = \rho \left(\frac{1}{2} |\boldsymbol{u}|^2 + \tilde{\boldsymbol{e}}\right), \ \tilde{\boldsymbol{p}} = \boldsymbol{p} + c_1^2 \rho$

$$\tilde{e}(\boldsymbol{F}) = \frac{c_1^2}{2} (\operatorname{tr}(\boldsymbol{F} \cdot \boldsymbol{A} \cdot \boldsymbol{F}^T) - d - \log |\boldsymbol{F} \cdot \boldsymbol{A} \cdot \boldsymbol{F}^T|) - \frac{d_1^2}{1 - \gamma} |\boldsymbol{F}|^{1 - \gamma}$$

Linking solids with fluids

Standard comparison tools for systems of balance laws *rigorously* link the fluid model (24) with (neo-Hookean) elastic *solid* bodies when $\frac{1}{\lambda} \rightarrow 0$ i.e. when no energy is dissipated [Boyaval 2023]

Whenever $0 < \lambda < \infty$, flows dissipate and one is considering non-ideal *fluids* with extra-stress

$$\lambda \left(\partial_t \boldsymbol{\tau} + (\boldsymbol{u} \cdot \boldsymbol{\nabla}) \boldsymbol{\tau} - \boldsymbol{\nabla} \boldsymbol{u} \cdot \boldsymbol{\tau} - \boldsymbol{\tau} \cdot \boldsymbol{\nabla} \boldsymbol{u}^{\mathsf{T}} + (\operatorname{div} \boldsymbol{u}) \boldsymbol{\tau} \right) = 2\mu \boldsymbol{D}(\boldsymbol{u}) - \boldsymbol{\tau}$$

When $\lambda \to 0$, fluids memory is fading infinitely fast and fluids become formally *Newtonian*, with non-zero viscosity $\mu = \lambda c_1^2$ if $c_1^2 \to \infty$ at the same time

Entropy and temperature

Thermal influences on mechanics were neglected so far

$$-\frac{\rho c_1^2}{2\lambda} (\boldsymbol{I} - \boldsymbol{c}^{-1}) : (\boldsymbol{c} - \boldsymbol{I}) \equiv \rho \theta (\partial_t + \boldsymbol{u} \cdot \boldsymbol{\nabla}) \eta =: \rho (\partial_t + \boldsymbol{u} \cdot \boldsymbol{\nabla}) \boldsymbol{e}_{\boldsymbol{s}}(\eta)$$

 \Rightarrow let *e* depend on η and preserve entropy production ?

If we assume $K(\theta)$ affine in a θ -convex Helmholtz free energy

$$\boldsymbol{e}^{\star}(\boldsymbol{F},\theta) = \frac{\kappa(\theta)}{2} \bar{\boldsymbol{e}}_{\boldsymbol{A}}(\boldsymbol{F}) + \psi_{0}(|\boldsymbol{F}|,\theta)$$
(26)

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where $\bar{e}_{A}(F) = tr(F \cdot A \cdot F^{T}) - d - \log |F \cdot A \cdot F^{T}|$, then

$$m{e}(m{F},\eta) = rac{K - heta \partial_{ heta} K}{2} ar{m{e}}_{m{A}}(m{F}) + m{e}_0\left(|m{F}|,\eta + \partial_{ heta} K \;ar{m{e}}_{m{A}}(m{F})
ight)$$

after Legendre transform of (26) is jointly convex in $(|\mathbf{F}|, \mathbf{F}, \eta)$, while $\boldsymbol{\sigma} = \rho K(\theta) \mathbf{F} \cdot \mathbf{A} \cdot \mathbf{F}^{T} - \tilde{p}(\rho, \theta) \mathbf{I}$ like [Dressler-Edwards-Öttinger 1999]

Adding heat transfer by conduction

Heat conduction at finite-speed can be added using

$$m{e}(m{F},\eta,m{p}) = rac{K- heta\partial_{ heta}K}{2}m{ar{e}}_{A}(m{F}) + m{e}_{0}\left(|m{F}|,\eta+\partial_{ heta}K\,ar{m{e}}_{A}(m{F})
ight) + rac{ au}{2}|m{p}|^{2}$$

$$au
ho(\partial_t + u^i \partial_i) oldsymbol{p} + \operatorname{div}(\zeta(heta)
ho oldsymbol{F}) =
ho heta |\zeta'(heta)|^2 \hat{\kappa}^{-1} oldsymbol{p}$$

as in pioneering works of Cattaneo,

with an additional heat flux in energy balance (25)

$$\partial_t \tilde{E} + \operatorname{div}\left(\tilde{E}\boldsymbol{u} - \boldsymbol{\sigma}\cdot\boldsymbol{u} + \theta\zeta'(\theta)\boldsymbol{p}\right) = \rho \boldsymbol{f}\cdot\boldsymbol{u}$$

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where $\tilde{E} = \rho \left(\frac{1}{2} |\boldsymbol{u}|^2 + \boldsymbol{e}(\boldsymbol{F}, \eta, \boldsymbol{p}) \right)$

Compatibility with Fourier's law

First, balance of energy $\hat{\rho}\partial_t e + \partial_\alpha Q^\alpha = \hat{\rho}r$ for $e(\eta, \mathbf{p})$ is compatible with second law $\hat{\rho}\theta\partial_t\eta + \theta\partial_{\alpha}q^{\alpha} - \hat{\rho}r = \hat{\rho}\mathcal{D} > 0$ when $Q^{\alpha} = \theta q^{\alpha}$, $\hat{\rho}(\partial_{p^{\alpha}} e) \partial_t p^{\alpha} + q^{\alpha} \partial_{\alpha} \theta = -\hat{\rho} \mathcal{D} < 0$ and $\rho C_{1}(\partial_{t} + u^{i}\partial_{i})\hat{\rho}\theta + \partial_{i}\left(\theta\rho F_{\alpha}^{i}\boldsymbol{q}^{\alpha}\right) = \rho\left(\hat{\rho}\mathcal{D} + F_{\alpha}^{i}\boldsymbol{q}^{\alpha}\partial_{i}\theta\right)$ (27)where $\theta := \partial_{\eta} e$, $C_1(\theta) := \theta(\partial_{nn}^2 e)^{-1}$, r = 0 implies Fourier's law $\theta \rho F^i_{\alpha} q^{\alpha} \to -\kappa_{ii} \partial_i \theta$ and $F^i_{\alpha} q^{\alpha} \partial_i \theta + \mathcal{D} \equiv q^{\alpha} \partial_{\alpha} \theta + \mathcal{D} \to \mathbf{0}$, i.e. $\theta \rho \boldsymbol{q} \to -\hat{\kappa}^{-1} \nabla_{\boldsymbol{a}} \theta$, $\hat{\rho} \mathcal{D} \to \theta \rho \boldsymbol{q}^T \hat{\kappa}^{-1} \boldsymbol{q} > 0$ ($\hat{\kappa} := \boldsymbol{F}^{-1} \kappa \boldsymbol{F}^T$) e.g. if $\tau \hat{\rho} \partial_t p^{\alpha} + \partial_{\alpha} \zeta(\theta) = -\rho \theta |\zeta'(\theta)|^2 [\hat{\kappa}^{-1}]_{\alpha\beta} p^{\beta}$, $\boldsymbol{p} = \boldsymbol{Q}/(\theta \zeta'(\theta))$

Extensions possible

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One can change the stored energy and introduce finite-extensibility:

$$\psi = \psi_0 + \mathcal{K}(\theta) b^2 \log \left(1 - \frac{F_\alpha^i F_\beta^i A^{\alpha\beta}}{b^2} \right) - k_B \theta \log |F_\alpha^i F_\beta^i A^{\alpha\beta}| + \frac{\tau}{2} |\mathbf{p}|^2$$

or add a term function of \hat{F} for 3D flows... or let λ vary (as a function of θ , **A**, **F**... or yet another structure parameter)

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1 Setting the constitutive modelling issue

Prom anisotropic elastodynamics to viscoelastic fluids



Saint-Venant for shallow flows:viscous?

Saint-Venant [1871]: free-surface gravity flows of depth H(t, x, y) > 0 are governed by hydrostatic pressure P = gH/2

$$\partial_t H + \operatorname{div}(H \boldsymbol{U}) = 0$$
 (28)

$$\partial_t(H\boldsymbol{U}) + \operatorname{div}(H\boldsymbol{U} \otimes \boldsymbol{U} + H(P + \Sigma_{zz})\boldsymbol{I} - H\boldsymbol{\Sigma}_h) = -kH\boldsymbol{U}$$
 (29)

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and $\boldsymbol{\Sigma} = 0$, or $\boldsymbol{\Sigma}_h = 2\nu D(\boldsymbol{U})$, $\boldsymbol{\Sigma}_{zz} = -(\boldsymbol{\Sigma}_{xx} + \boldsymbol{\Sigma}_{yy})$

2D shallow elastodynamics

 $\lambda \to \infty$: elastodynamics for thin layers $H \equiv F_c^z = |F_h|^{-1} > 0$ of hyperelastic materials with deformation $F = \partial_{a,b,c}(x, y, z)$

$$\partial_t \boldsymbol{F} + (\boldsymbol{u} \cdot \boldsymbol{\nabla}) \boldsymbol{F} = (\boldsymbol{\nabla} \boldsymbol{U}) \boldsymbol{F}$$

and with a Hookean stress function of $\boldsymbol{B} = \boldsymbol{F} \boldsymbol{F}^{T}$

$$\boldsymbol{\Sigma}_{h} = \partial_{\boldsymbol{F}_{h}} \left(\frac{G}{2} \boldsymbol{F}_{h} : \boldsymbol{F}_{h} \right) \boldsymbol{F}_{h}^{T}, \quad \boldsymbol{\Sigma}_{zz} = \partial_{\boldsymbol{F}_{c}^{z}} \left(\frac{G}{2} |\boldsymbol{F}_{c}^{z}|^{2} \right) \boldsymbol{F}_{c}^{z}$$

i.e. $\boldsymbol{\Sigma}_h - \boldsymbol{\Sigma}_{zz} \boldsymbol{I} \equiv \boldsymbol{G}(\boldsymbol{B}_h - \boldsymbol{B}_{zz} \boldsymbol{I}) = (\partial_{\boldsymbol{F}_h} \boldsymbol{e}) \boldsymbol{F}_h^T;$

in fact is as *symmetric hyperbolic* system of conservation laws with *polyconvex* energy $e := \frac{g}{2} |\mathbf{F}_h|^{-1} + \frac{G}{2} (\mathbf{F}_h : \mathbf{F}_h + |\mathbf{F}_h|^{-2})$

2D shallow elastodynamics SCL

When $\lambda \rightarrow \infty$, SV-UCM should be

$$\begin{aligned} \partial_t (HF^i_{\alpha}) + \partial_j (HU^j F^i_{\alpha} - HF^j_{\alpha} U^i) &= 0\\ \partial_t (HU^i) + \partial_j (HU^j U^i + gH^2/2 + GH^3 - GHF^i_{\alpha} F^j_{\alpha}) &= -KHU^i \end{aligned}$$

as long as $\partial_{\alpha}(\sigma_{\alpha\beta}F_{\beta}^{k}) = 0$, $\partial_{j}(HF_{\alpha}^{j}) = 0$ (Piola) so e.g.

$$\partial_t H + \partial_j (H U^j) = 0.$$

It is possible accomodate viscosity using "memory" variables.

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2D viscoelastic Saint-Venant

Adding $A_{\alpha\beta}$ to the usual dependent variables yields

$$\begin{aligned} \partial_t H + \partial_j (HU^j) &= 0\\ \partial_t (HF^i_{\alpha}) + \partial_j (HU^j F^i_{\alpha} - HF^j_{\alpha} U^j) &= 0\\ \partial_t (HU^i) + \partial_j (HU^j U^i + gH^2/2 + GH^3 A_{cc} - GHF^i_{\alpha} A_{\alpha\beta} F^j_{\beta} F^j_{\alpha}) &= -KHU^i\\ \partial_t (HA_{\alpha\beta}) + \partial_j (HU^j A_{\alpha\beta}) &= H(|\mathbf{F}_h|^{-2} \sigma_{\alpha\alpha'} \sigma_{\beta\beta'} F^k_{\alpha'} F^k_{\beta'} - A_{\alpha\beta})/\lambda\\ \partial_t (HA_{cc}) + \partial_j (HU^j A_{cc}) &= H(H^{-2} - A_{cc})/\lambda \end{aligned}$$

i.e. a system of conservation laws, with companion law

 $\begin{aligned} &\partial_t (HE) + \partial_x \left(HEU + H(P + \Sigma_{zz} - \Sigma_{xx})U - H\Sigma_{xy}V \right) \\ &+ \partial_y \left(HEV - H\Sigma_{yx}U + H(P + \Sigma_{zz} - \Sigma_{yy})V \right) \leq -KH |\boldsymbol{U}|^2 - HD \end{aligned}$

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Computing solutions

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 $au := \sigma + p \, \delta$ satisfies a *compressible UCM* eq.

 $\lambda \stackrel{\nabla}{\tau} + \tau (\operatorname{div} \boldsymbol{u}) + \tau = 2\mu \boldsymbol{D}(\boldsymbol{u})$

using $\stackrel{\nabla}{\boldsymbol{\tau}}:=\partial_t\boldsymbol{\tau}+(\boldsymbol{u}\cdot\boldsymbol{\nabla})\boldsymbol{\tau}-\boldsymbol{\nabla}\boldsymbol{u}\,\boldsymbol{\tau}-\boldsymbol{\tau}\,\boldsymbol{\nabla}\boldsymbol{u}^{\mathsf{T}}$

Assuming 1D flow, one retrieves the damped-wave equation

$$\lambda \partial_{tt}^2 \tau(t, y) + \partial_t \tau(t, y) = \mu \partial_{yy}^2 \tau(t, y)$$

with shear-wave solution to Stokes first-problem in $\{y > 0\}$



But beyond ?

Perspectives

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- · Vorticity generated locally in an initially-quiescent fluid
- Fluid-Solid contact "seamlessly" modelled (discontinuity)
- · Rheology: local re-structuration under shear

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1D case (Stoker): *h* ; $\mu = 1$ and 10, $\lambda = \infty$



1D case (Stoker): τ_{xx}, τ_{zz} ; $\mu = 1, \lambda = \infty$



1D case (Stoker): τ_{xx}, τ_{zz} when $\mu = 10$, $\lambda = \infty$



Stoker "dam-break" benchmark test case

Compute a solution for $t \in (0, .2)$ in $(x, y) \in [0, 1]^2$ starting from

$$(H, U, V, B_{xx}, B_{yy}, B_{xy}, B_{zz}) = \begin{cases} (3, 0, 0, 1, 1, 0, 1) & x + y < 1 \\ (1, 0, 0, 1, 1, 0, 1) & x + y > 1 \end{cases}$$

SV-UCM Depth *H* T = .2Froude $g^{-1/2} = .3$ Elasticity $G = 10 \approx g$ Weissenberg $\lambda = 1 \gg T$



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Varying elasticity G = .1, 1, 10 at g = 10

Depth *H* (top) and strain B_{xx} (bottom) at T = .2 for $\lambda = .01, .1, 1$



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Varying elasticity G = .1, 1, 10 at g = 10



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Varying Froude g = 1, 10, 100

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Depth *H* at T = .2 for $\lambda = .01$ (top) and .1 (bottom) with elasticity G = 1 (left) and 10 (right)



2D column "circular dam-break" benchmark

Solution at T = .2 in $(x, y) \in [0, 1]^2$ starting from

 $(H, U, V, B^{xx}, B^{yy}, B^{xy}, B^{zz}) = \begin{cases} (3, 0, 0, 1, 1, 0, 1) & (x - .5)^2 + (y - .5)^2 < .2\\ (1, 0, 0, 1, 1, 0, 1) & (x - .5)^2 + (y - .5)^2 > .2 \end{cases}$



 $g = 10, G = 0.01, \lambda = 1$ at T = .2



$g = 10, G = 1, \lambda = 1$ at T = .2



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